Comparative Analysis of Flat Cube Reflectors for Automotive Safety to Meet Regulatory Standards of US Society of Automotive Engineers and EU Economic Commission for Europe

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Abstract - To establish a foothold in the global market for traffic safety reflective signs, it is essential to develop a flat cube reflector that adheres to the regulatory standards set by both the United States Society of Automotive Engineers (SAE) and the Economic Commission for Europe (ECE). These standards primarily differ in terms of the specified observation angle and reflector value, with SAE requiring an observation angle of 0.2 degrees and ECE mandating 0.33 degrees. Leveraging sophisticated software tools, including SolidWorks, TracePro, Speos, LightTools, and Optiswork, allows for the meticulous optimization of the flat cube reflector to maximize its reflectivity. This optimization involves the precise arrangement of pins within the reflector, oriented unidirectionally.

Received: 24 October 2023. Revised: 31 January 2024. Accepted: 04 March 2024. Published: 28 May 2024. Our findings highlight the innovative potential of a singular flat cube reflector design that can simultaneously meet the stringent standards of both SAE and ECE. This dual-compliance capability holds significant promise for cost savings in the production of reflex reflectors intended for the European and American automobile markets.

Keywords – Reflective sign, traffic safety, flat cube reflector, regulatory standards.

1. Introduction

In today's fiercely competitive global market for traffic safety equipment, meeting regulatory standards is paramount for industry players. This imperative drives the development of flat cube reflectors that adhere rigorously to the criteria outlined by both the United States Society of Automotive Engineers (SAE) and the Economic Commission for Europe (ECE). These standards, which intricately detail observation angles and reflector values, highlight the critical need for precise and compliant design in reflective sign production [1], [2].

At the core of this endeavor lies the flat cube reflector, a pivotal component widely employed across diverse applications such as warning signs, street markers, and parking facility indicators. These reflectors play a crucial role in bolstering visibility under low-light conditions, aiding in the swift identification of objects for motorists. Crafted from an array of materials ranging from glass and plastic to polycarbonate and metal, each reflector is meticulously engineered to redirect light in a specific direction.

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Leveraging innovative design methodologies and cutting-edge software tools, manufacturers strive to optimize flat cube reflectors, ensuring maximal reflectivity to meet the exacting standards set forth by both SAE and ECE [3].

This paper embarks on a journey into the realm of flat cube reflector design and optimization, guided by the insights gleaned from Figures 1, 2, and 3. Figure 1 illustrates the fundamental principle of reverse reflection inherent in flat cube reflectors, elucidating how incident light is redirected back towards its source a pivotal mechanism in enhancing nighttime visibility. Complementing this, Figure 2 showcases the versatile applications of flat cube reflectors, spanning from road pavements to vehicular surfaces, underscoring their ubiquitous presence in the realm of traffic safety. Moreover, Figure 3 delves deeper into the intricate geometry of cube reflectors, illustrating the convergence of angles and surfaces critical to their reflective efficacy [4], [5], [6].

Through an amalgamation of simulation techniques and empirical analysis, this study endeavors to unlock the optimization potential encapsulated within flat cube reflectors. By decoding the nuances encapsulated in these figures, we aim to chart a course towards dual compliance with SAE and ECE standards, paving the way for enhanced safety and efficiency in automotive environments.



Figure 1. The principle of reverse reflection for flat cube reflector



Figure 2. The flat cube reflector is used on pavements, traffic signs, vehicles and clothing



Figure 3. (a) Cat-eye reflective glasses; (b) Cubic angle reflector

2. Method of Experience

Research methodology unfolds in a meticulously structured manner, blending computational modeling with empirical validation to unravel the intricacies of flat cube reflector optimization while aligning with the stringent regulatory standards set by both the United States Society of Automotive Engineers (SAE) and the Economic Commission for Europe (ECE). This methodological journey is characterized by a series of sequential steps, each meticulously designed to shed light on the optimal design parameters essential for achieving dual compliance [7], [8], [9], [10]. Central to the approach is the utilization of cutting-edge software tools, including SolidWorks, TracePro, Speos, LightTools, and Optiswork. These tools serve as invaluable assets, facilitating the intricate process of reflector design, simulation, and analysis with unparalleled precision and efficiency.

The study begins with an in-depth exploration of reflector geometry, drawing inspiration from the fundamental principles of light transmission depicted in Figure 4. By meticulously manipulating dihedral angles and surface configurations within flat cube reflectors, we seek to unlock the full potential of these reflective devices while ensuring alignment with prescribed observation angles and reflector values mandated by regulatory standards.

Each surface configuration undergoes rigorous scrutiny, with a keen focus on optimizing reflector parameters to maximize reflective efficiency. Through iterative refinement and meticulous adjustment of design variables, we strive to inch closer towards the elusive threshold of dual compliance with SAE and ECE standards [11], [9] [12], [13], [14].

Complementing our computational endeavors is a parallel track of empirical validation, wherein realworld experiments are conducted to corroborate the findings gleaned from simulation studies. These empirical investigations serve as crucial litmus tests, validating the efficacy of our computational models and providing invaluable insights into the practical feasibility of optimized reflector designs. Throughout this methodological journey, attention to detail reigns supreme, with each design iteration and experimental trial meticulously documented and analyzed. By embracing a holistic approach that synthesizes computational modeling with empirical validation, we aim to transcend conventional boundaries and chart a path towards innovation and excellence in reflective sign design.

Our methodological framework encapsulates a symbiotic blend of computational prowess and hands-on experimentation, underpinned by a relentless pursuit of precision and excellence. Through this integrative approach, we endeavor to push the boundaries of reflective sign design, ushering in a new era of safety and efficiency in automotive environments.

We consider three angles: α , β , and γ , all exceeding 90 degrees. When these three planes converge to form a reflective cube, as depicted in Figure 5, the dispersion of the cube reflector's beam is contingent upon the angle offset. This dispersion can be calculated using Formula (1) and is depicted in Figure 6. Notably, the cube reflector achieves its maximum beam dispersion when the angle offset equals 90 degrees. This suggests that the reflector is most adept at redirecting light towards its source when the angle offset is precisely 90 degrees. Conversely, as the angle offset surpasses 90 degrees, the beam dispersion diminishes, signifying a decrease in the reflector's efficiency in redirecting light back towards its source. By manipulating the angle offset, it becomes feasible to modulate the light intensity emitted by the cube reflector. This capability renders cube reflectors invaluable tools for augmenting object visibility in low-light environments.



Figure 4. The definition of the three target-fixed axes and the three dihedral angles



Figure 5. The relationship between the angle and the surface plane

$$\theta = \frac{4}{2}\sqrt{6}n\delta \tag{1}$$

Where:

+ n is the corner cube index of refraction

 $+\,\delta$ is the angle by which the dihedral angles exceed 90°

 $+ \theta$ is the angle between the incident and the reflected rays.



Figure 6. Design and simulation results by SolidWorks and TracePro with surface A



Figure 7. The design and simulation outcomes generated by SolidWorks and TracePro, specifically pertaining to surface B



Figure 8. The design and simulation findings conducted using SolidWorks and TracePro, highlighting surface C



Figure 9. The design of a flat plant cube retroreflector, created using SolidWorks



Figure 10. Simulation results obtained from the software TracePro

3. Results and Discussion

In an ideal flat cube retroreflector, each pair of reflecting faces forms a perfect 90-degree angle, resulting in the reflected beam being precisely opposite in direction to the incident beam. However, if even one, two, or all three of the dihedral angles deviate slightly from 90 degrees, the reflected beam will split into two, four, or six separate beams, respectively. Each distinct beam corresponds to a specific order of reflection, as detailed in Table 1.

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δ1= δ2 (Degree)	δ₃ (Degree)	$\theta_{1=}\theta_{2}$ (Degree)	θ₃ (Degree)
0	0	0	0
0.01	0.02	0.038	0.04
0.02	0.02	0.067	0.067
0.03	0.02	0.087	0.079
0.04	0.02	0.127	0.102
0.05	0.02	0.144	0.113
0.06	0.02	0.182	0.135
0.07	0.02	0.2	0.15
0.08	0.02	0.225	0.160
0.09	0.02	0.26	0.18
0.10	0.02	0.28	0.19
0.11	0.02	0.33	0.2
0.12	0.02	0.35	0.21
0.13	0.02	0.36	0.24
0.14	0.02	0.4	0.26
0.15	0.02	0.42	0.28
0.16	0.02	0.44	0.29

Table 1. The angle between the incident and the reflected rays

The research findings illustrate that when $\delta 1$ and $\delta 2$ both equal 0.11° and $\theta 1$ and $\theta 2$ both equal 0.2°, adhering to SAE regulations, and when $\delta 3$ equals 0.02° and $\theta 3$ equals 0.33°, complying with ECE regulations, the reflected beam undergoes division into two, four, or six beams.

The experimentation reveals the intricate relationship between the angles of reflection within a prism. As depicted in Figure 15, adjustments in these angles are crucial for achieving compliance with the EU ECE standard of 0.33° . This adjustment is visually represented in Figure 10, showcasing the manipulation of bright spots within the prism. The experiment highlights distinct scenarios based on the relationships between α , β , and γ angles:

- If α=β=γ, with all angles exceeding 90 degrees, the reflector configuration is considered regular, as illustrated in Figure 11(a-b).
- When α=β and γ is larger (γ> α=β), the reflector configuration aligns with either ECE or SAE standards, as depicted in Figure 12(a-b).
- Finally, if α=β is larger and γ is smaller (γ< α=β), the reflector configuration complies with both ECE and SAE standards, as shown in Figure 13(a-b).
- In the case where all three angles $\alpha=\beta=\gamma$ equal 90 degrees, the reflector configuration is characterized as having right angles.



Figure 11a. The experimental results of the Regular Flat Reflex reflector compliant with ECE standards



Figure 11b. The Regular Flat Reflex reflector compliant with SAE standards



Figure 12. The Flat Reflex reflector conforming to ECE standards



Figure 12b. The Flat Reflex reflector meeting SAE standards



Figure 13a. Flat Reflex reflector designed to meet the specifications of both the Society of Automotive Engineers (SAE) and the Economic Commission for Europe (ECE)



Figure 13b. Flat Reflex reflector designed to meet the specifications of both the Economic Commission for Europe (ECE) and the Society of Automotive Engineers (SAE)

Regarding the dihedral angle in a corner cube, a retro reflector formed with three planes is considered first then the coordinate system is defined as shown in Figure 14. The differences between the right angles are defined by $\delta x'$, $\delta y'$ and $\delta z'$ as shown in Fig 15.



Figure 14. Relationship between three angles, six points and three planes



Figure 15. Definition of dihedral angles

4. Conclusion

Throughout this research endeavor, our primary objective has been to enhance the efficiency of planar reflectors, focusing on two distinct categories: flat cube reflectors and configurations of cubes arranged in parallel to form a reflective plane. Our central aim has been to optimize the reflective capabilities of these structures, with specific attention given to incident light angles of 0.2 degrees and 0.33 degrees, in alignment with regulatory standards set by SAE and EU ECE.

Simulation studies conducted across three planes involving the cube configuration have revealed the intricate relationship between reflective angles and efficiency. By manipulating angles within these planes, we have demonstrated precise control over the reflective angle of light, highlighting the significant influence of reflective plane geometry on reflection efficiency.

It is imperative to acknowledge the limitations of our investigation, notably the exclusion of curved surfaces from our study. However, future research endeavors will address this limitation, paving the way for a comprehensive understanding of reflective surface geometry and its impact on efficiency.

Our research agenda encompasses а multifaceted investigation into factors influencing plane reflection efficiency. This includes exploring variables such as surface roughness and material selection to discern their impact on reflectivity. Additionally, we aim to examine the influence of spatial separation between the reflector and light source on reflective efficiency, further enriching our understanding of reflective surface dynamics. Moreover, our inquiry extends to the exploration of alternative reflector configurations, aiming to identify designs that offer enhancements in plane reflection efficiency beyond the scope of traditional flat surfaces. Through these ongoing research endeavors, we seek to advance the field of reflective sign design, unlocking new insights and innovations to elevate safety and efficiency in automotive environments.

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